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Progress Review

Thermomechanical fatigue of Boeing 60-NiTi

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Progress overview

- Cumulative results for water jet processed SMA strips
- First results for EDM processed SMA strips Problems related to heat treatment performed in air vs. in vacuum
- Influence of environment during heat treatment on fracture surfaces
- Recommendations for further testing





Cumulative results for water jet

processed SMA strips





After testing all water jet processed specimens and after identification of erroneous data due to experimental malfunctions (creep-like behavior, grip slip, non-uniform test gauge of specimens), 4 tables were generated to collect the testing parameters such as: and also significant generated data:

- Specimen number
- Specimen thickness
- Applied stress level

and also significant generated data such as:

- Recoverable strain half way through the life of the specimens
- Plastic strain half way through the life of the specimens
- Recoverable strain at failure
- Plastic strain at failure



Comprehensive results for water jet processed specimens for heat treatment #1



Table 1 is ordered according to increasing sample thickness

HT1 - 1 hr @ 850°C, 1 hr @ 450°C							
Specimen	Thickness	Applied stress	Cycles to failure	Recoverable strain	Plastic strain	Recoverable strain	Plastic strain
number	(mils)	(MPa)	Nf	@ 1/2 Nf	@ 1/2 Nf	@ Nf	@ Nf
3	5	204	6896	0.01073	0.00257	0.01063	0.00685
10	5	100	67571	0.00464	0.00861	0.0046	0.01457
2	10	250	3838	0.01209	0.02585	0.01329	0.03511
5	10	90	57598 (run out)	0.00583	0.01337	0.0048	0.0323
7	15	243	5251	0.0106	0.026	0.0104	0.03667
9	15	100	55811	0.00383	0.00726	0.00427	0.01074
1	Damaged during preliminary testing						
4	Invalid results (computer malfunction)						
6	MTS tested						
8	Invalid results (computer malfunction)						

Table 2 is ordered according to increasing applied stress level

HT1 - 1 hr @ 850°C, 1 hr @ 450°C							
Specimen	Thickness	Applied stress	Cycles to failure	Recoverable strain	Plastic strain	Recoverable strain	Plastic strain
number	(mils)	(MPa)	Nf	@ 1/2 Nf	@ 1/2 Nf	@ Nf	@ Nf
5	10	90	57598 (run out)	0.00583	0.01337	0.0048	0.0323
9	15	100	55811	0.00383	0.00726	0.00427	0.01074
10	5	100	67571	0.00464	0.00861	0.0046	0.01457
3	5	204	6896	0.01073	0.00257	0.01063	0.00685
7	15	243	5251	0.0106	0.026	0.0104	0.03667
2	10	250	3838	0.01209	0.02585	0.01329	0.03511
1	Damaged during preliminary testing						
4	Invalid results (computer malfunction)						
6	MTS tested						
8	Invalid results (computer malfunction)						

Remarks: Specimen #3 HT1 has a relatively small amount of accumulated plastic strain compared to the rest of the specimens



Comprehensive results for water jet processed specimens for heat treatment #2



Table 1 is ordered according to increasing sample thickness

HT2 1 hr @ 850°C, 20 hrs @ 450°C							
Specimen	Thickness	Applied stress	Cycles to failure	Recoverable strain	Plastic strain	Recoverable strain	Plastic strain
number	(mils)	(MPa)	Nf	@ 1/2 Nf	@ 1/2 Nf	@ Nf	@ Nf
4	5	107	18338	0.0067	0.01406	0.00734	0.01926
5	5	103	58341 (run out)	0.00495	0.01676	0.00425	0.01901
7	5	250	3035	0.01123	0.00956	0.01063	0.01669
6	10	226	8897	0.00955	0.01154	0.00895	0.02059
9	10	100	41463	0.00384	0.01581	0.00424	0.02473
10	10	250 creep like behavior - slip in grips					
3	15 142 creep like behavior - slip in grips						
1	Damaged during preliminary testing						
2	Not applicable for isobaric uniaxial fatigue testing - irregular cross section with major notches						
8	MTS tested						

Table 2 is ordered according to increasing applied stress level

HT2 1 hr @ 850°C, 20 hrs @ 450°C							
Specimen	Thickness	Applied stress	Cycles to failure	Recoverable strain	Plastic strain	Recoverable strain	Plastic strain
number	(mils)	(MPa)	Nf	@ 1/2 Nf	@ 1/2 Nf	@ Nf	@ Nf
9	10	100	41463	0.00384	0.01581	0.00424	0.02473
5	5	103	58341 (run out)	0.00495	0.01676	0.00425	0.01901
4	5	107	18338	0.0067	0.01406	0.00734	0.01926
3	15	142	creep like behavior - slip in grips				
6	10	226	8897	0.00955	0.01154	0.00895	0.02059
7	5	250	3035	0.01123	0.00956	0.01063	0.01669
10	10 250 creep like behavior - slip in grips						
1	Damaged during preliminary testing						
2	Not applicable for isobaric uniaxial fatigue testing - irregular cross section with major notches						
8	MTS tested						

Remarks: Specimen #7 HT2 has a relatively small amount of accumulated plastic strain compared to the rest of the specimens



Stress – life updated









Plastic strain at failure - Updated







Presentation of first results EDM processed SMA strips







EDM SP#1 HT1 - Thickness = 15 mils Non-Polished - 250MPa





5 mils thick EDM Specimens under 100 MPa constant stress.







5 mils thick EDM Specimens under 150 MPa constant stress.



Stain vs. Life of EDM specimens compared to Strain vs. Life of water jet specimens for thickness = 5 mils

- EDM Specimens
 - 100 MPa
 - HT A1: 949 cycles
 - HT A2: 2039 cycles
 - 150 MPa
 - HT A1: 1588 cycles
 - HT A2: 1917 cycles

- Water Jet Specimens
 - 100 MPa
 - HT A1: 67571 cycles
 - HT A2: 18338 cycles
 - 150 MPa
 - HT A1: 6896 cycles (200 MPa)
 - HT A2: 58341 cycles (103MPa)









Influence of environment during heat treatment on fracture surfaces





- Recall initial optical microstructural analysis for identification of possible failure modes
- Presentation of EDM processed specimens fracture surfaces to assess existence of oxide layer
- Conclusions on the presence of consequential oxide layer



- Influence of thickness can be seen as cracks are generated in the transverse direction of SP#3 HT1 where PS#7 HT1 displays more of a bulk behavior
- Different failure behavior from thickness 5 mils to 15 mils







- Transverse cracks and transverse tear up strong dependency on the width to height ratio
- Propagation of fatigue lines in a transverse pattern







- Thicker specimens display bulk behavior with multi-axial fatigue damage and propagation
- Notice the non-existence of contrasted surface layer: heat treatment performed in vacuum

SP#6 HT2 – thickness = 10 mils









 EDM specimens failing too early under 100MPa and 150MPa applied stress led to analysis of oxide layer due to heat treatment performed in air vs. in vacuum

Nf (HT in air, 100 -150 MPa) < 2000 cycles

Nf (HT in vacuum, 100 - 150 MPa) ≈ 50000 cycles



SP#6 HT1 – thickness = 5 mils

SP#8 HT2 - thickness = 5 mils









- Similar transverse fatigue lines with crack propagation along the same direction
- Significant contrasted surface layer on the specimens: initial oxide layer formed upon heat treatment. Interface is clear and cracks can be identified







• Specimens with minimum thickness (5 mils), failed very early due to a significant oxide layer contributing to crack initiation and to embrittlement

SP#8 HT2 – thickness = 5 mils









Recommendations for further testing





- Selection of heat treatment for better control over fatigue experiments and to enhance time to achieve fatigue testing: Heat Treatment 2
- Stress range to perform fatigue testing needs to be adjusted to
 100 150 250 MPa
- Selection of ideal thickness for best material response is to be
 15 mils (20 mils if stress range reduced to 100 150 200 MPa)
- Modification of actual test matrix to account for suggested modifications



Latest test matrix



Chosen Heat Treatment	A2*	
Chosen Specimen Thickness	.015 in.	(.381 mm)

Test Matrix							
Stress Applied (MPa)	Polished Specimens	Non-Polished Specimens					
100	3	3					
150	3	3					
250	3	3					

*HT #2 = 1 hr 850 C, furnace cool, 20 hrs 450 C, water quench.

Currently 18 new specimens will be needed: 9 polished

9 non-polished