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Department of Mechanical Engineering



# Effects of Severe Plastic Deformation and Sc Addition on the Recoverability of TiNiPd High Temperature Shape Memory Alloys

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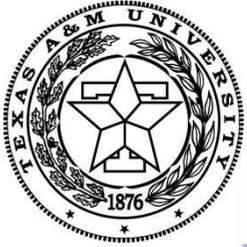


# Outline

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- Challenges
- Objectives
- Materials Processing
- Experimental Results
  - Material Characterization
  - Thermo-mechanical Testing
- Conclusion
- Future Work



# Challenges

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Conventional TiNi ~ 100°C

Ti(Ni,Pd) ~ 100-400°C

Operating Temperature  Challenges 

*Long term stability*

- Microstructure (recovery, recrystallization)
- Phase structure (decomposition)
- Resistance to oxidation

*Plasticity*

- Resistance to dislocation slip (ease of dislocation motion and decrease in the critical stress for slip)



# Objectives

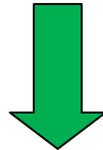
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Enhance the recoverability of a  $\text{Ti}_{50.5}\text{Ni}_{24.5}\text{Pd}_{25}$  (at. %) HTSMA



**Increase the resistance to dislocation slip**



Quaternary alloying with 0.5 at. % Sc (by solid solution hardening)

- Strong site preference for Ti
- Increases the formation energy, significantly affecting the bond strength in the alloy
- Increases the lattice parameter, thus the internal strain



Severe plastic deformation using equal channel angular extrusion (ECAE)

- Grain refinement
- Work hardening



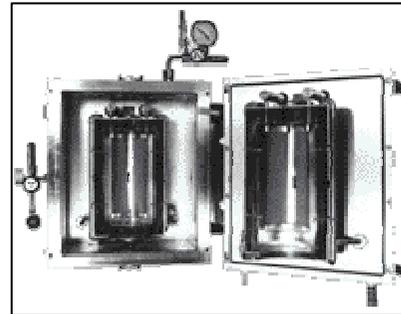
# Materials Processing

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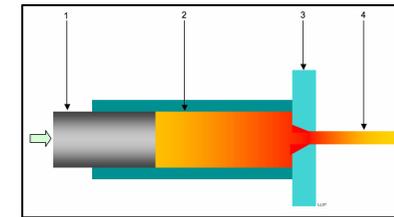
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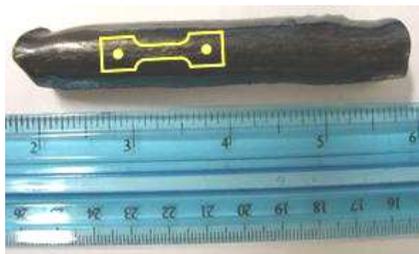
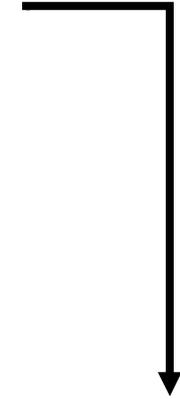
1. Vacuum induction melting of elemental constituents (Ni, Ti, Pd, Sc)



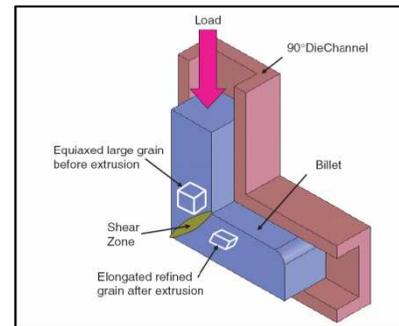
2. Homogenization of ingots at 1050°C for 72 hours



3. Extrusion at 900°C with an area reduction ratio of 7:1



5. Preparation of microtensile specimens from the as-extruded and ECAE'd billet by electrical discharge machining (EDM)



4. Severe plastic deformation of the as-extruded billet via ECAE



As-extruded Billet





# Experimental Results

## Part I

Addition of 0.5% Sc to the as-extruded

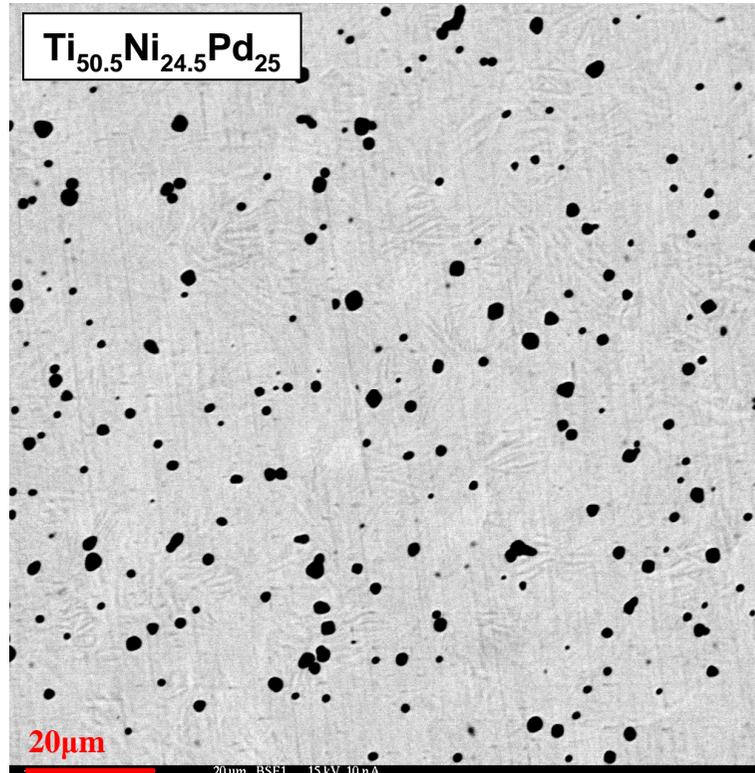




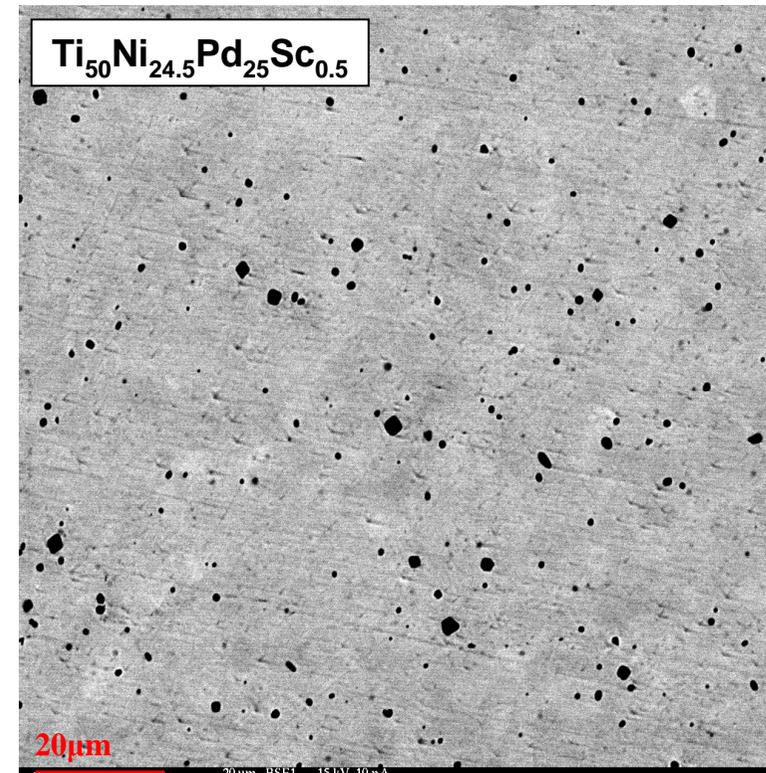
# Material Characterization

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Grain size  $\approx 5 - 15\mu\text{m}$  (Avg.  $10\mu\text{m}$ )  
Volume fraction of precipitates  $\approx 3.4\%$   
Average particle size  $\approx 1.48 \pm 0.58\mu\text{m}$



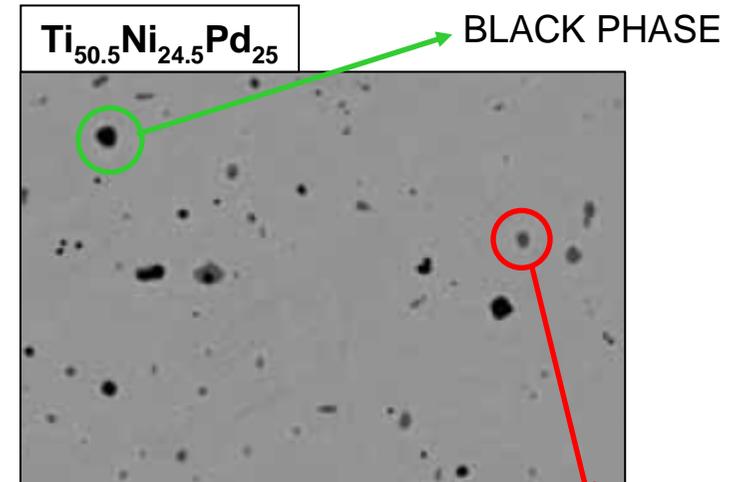
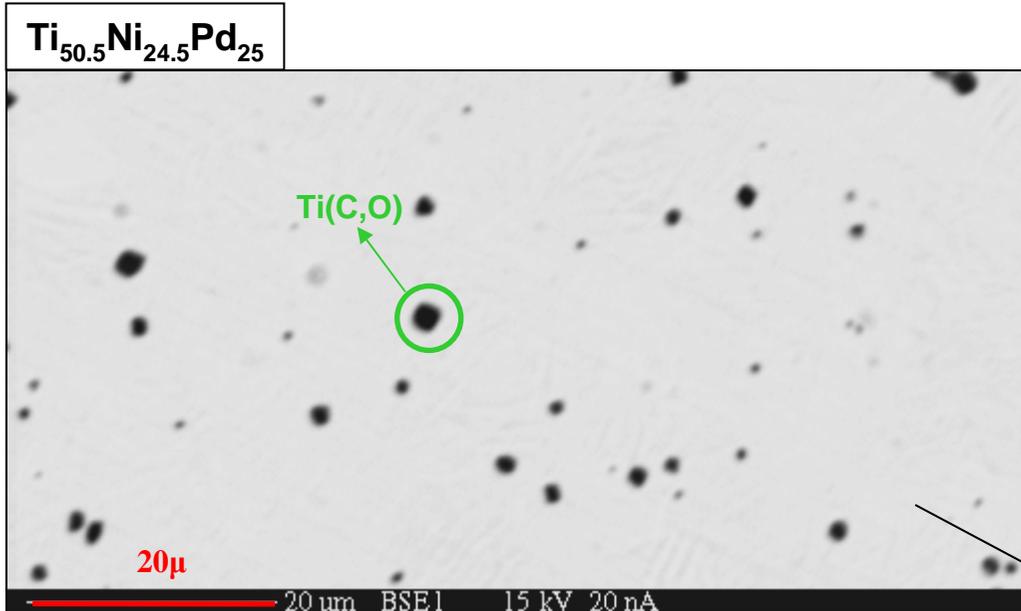
Grain size  $\approx 5 - 10\mu\text{m}$  (Avg.  $7\mu\text{m}$ )  
Volume fraction of precipitates  $\approx 1.4\%$   
Average particle size  $\approx 0.94 \pm 0.44\mu\text{m}$



# Material Characterization

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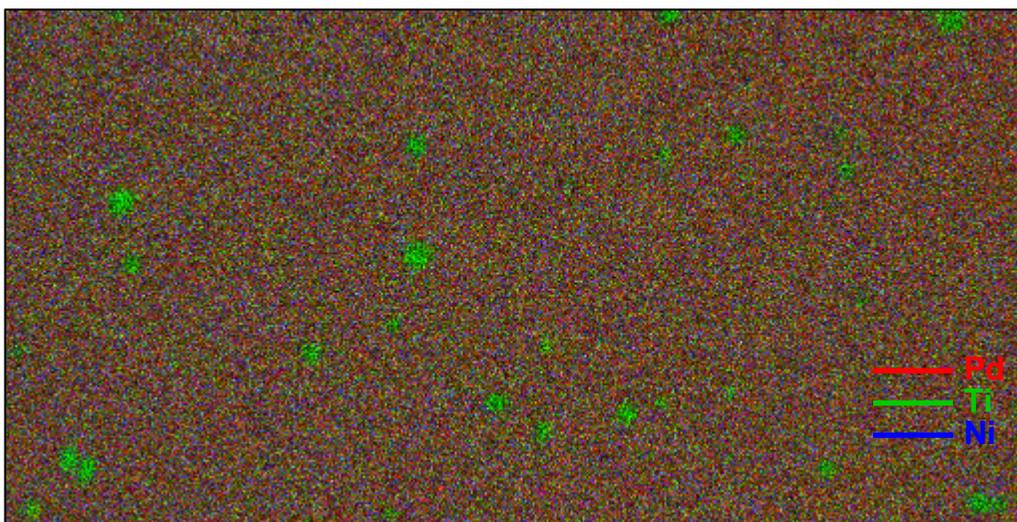
Glen Bigelow, M.S. Thesis

$Ti_2(Ni,Pd)$

Barely visible gray phases. Hard to define the composition with EDS.

## Matrix Composition from WDS Analysis

	Ti	Ni	Pd
at. %	49.62 $\pm 0.5$	24.42 $\pm 0.25$	25.96 $\pm 0.25$

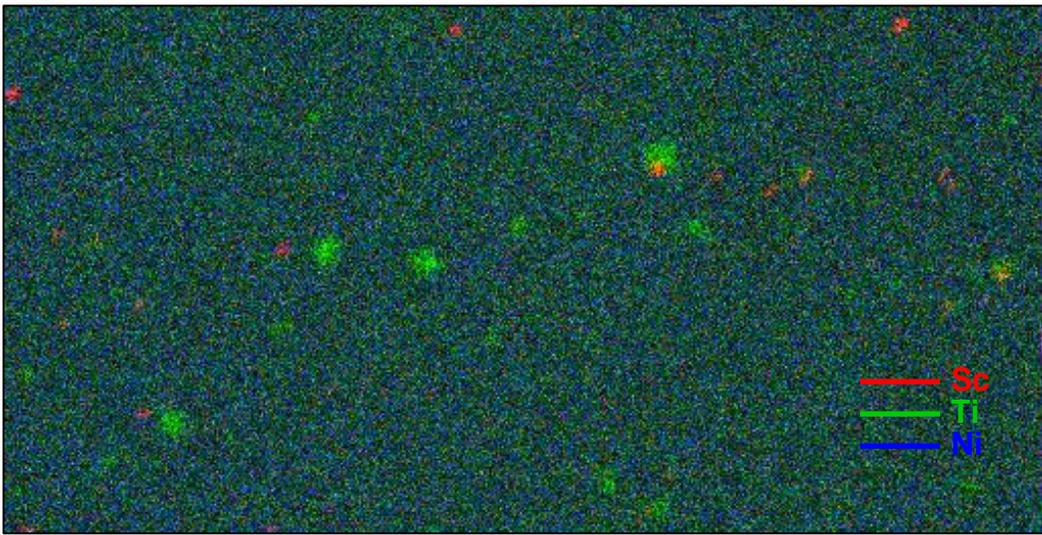
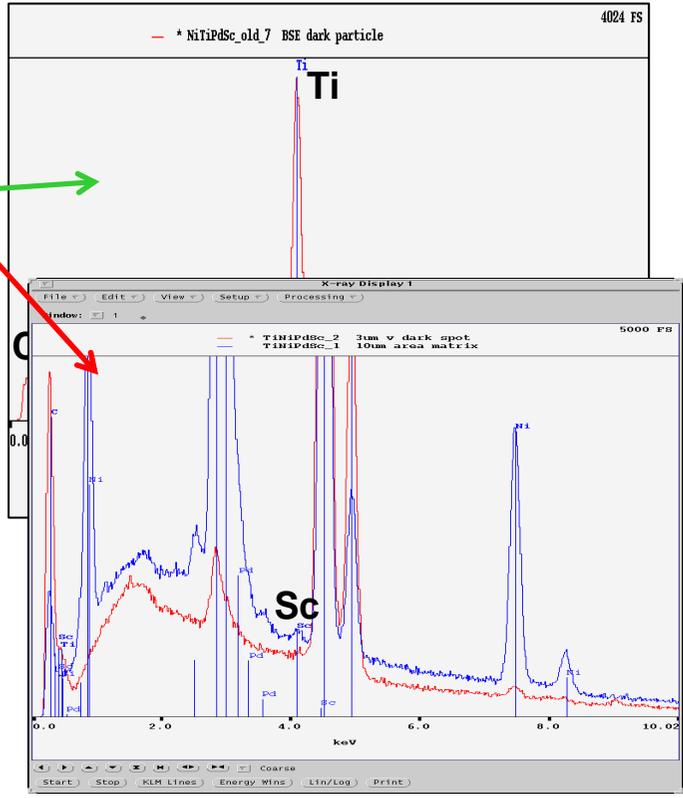
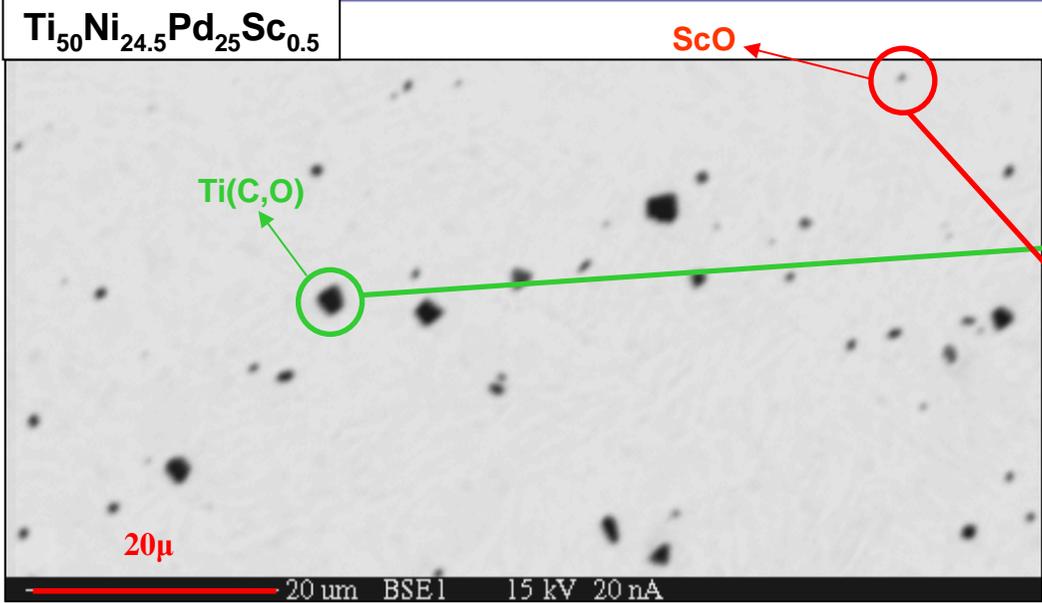




# Material Characterization

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Matrix Composition from WDS Analysis

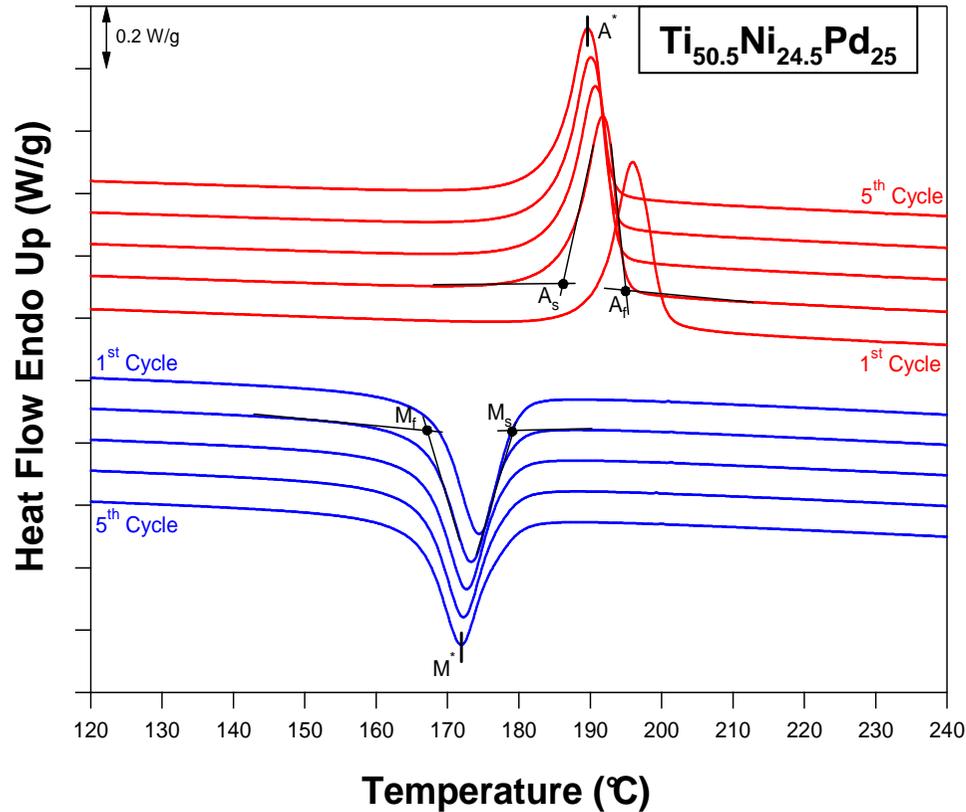
	Ti	Ni	Pd	Sc
at. %	49.41	25.11	25.02	0.46
	±0.5	±0.25	±0.25	±0.05



# Thermo-mechanical Testing

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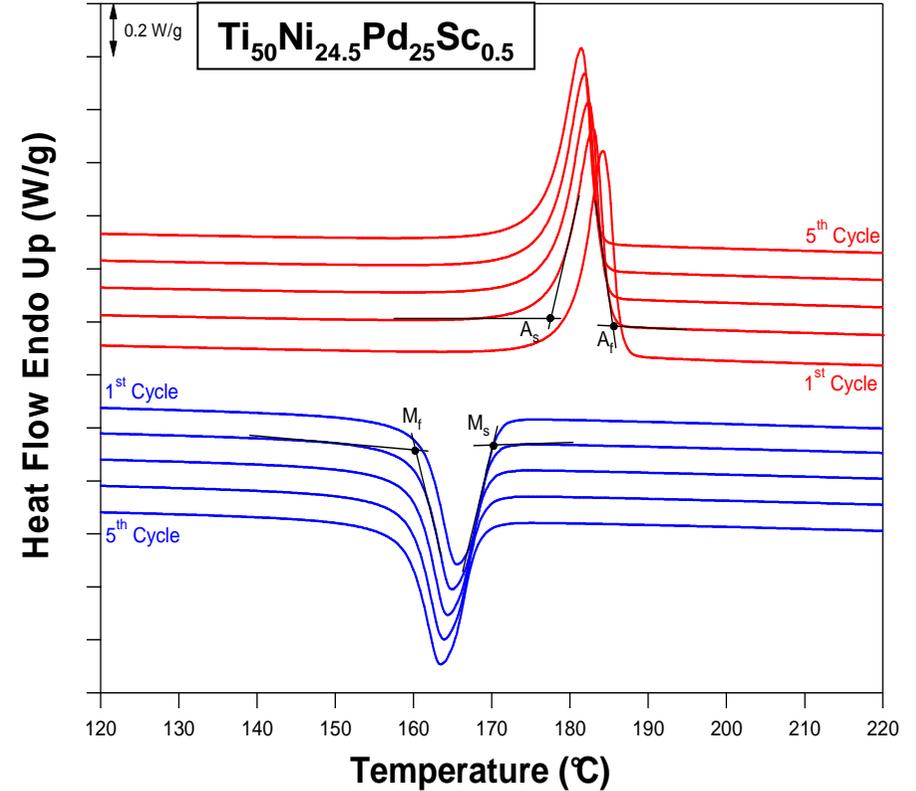
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$$M_s = 179.4^\circ\text{C}$$

$$A_f = 195.1^\circ\text{C}$$

Decreased transformation temperatures



$$M_s = 170.1^\circ\text{C}$$

$$A_f = 185.1^\circ\text{C}$$

Increased cyclic stability

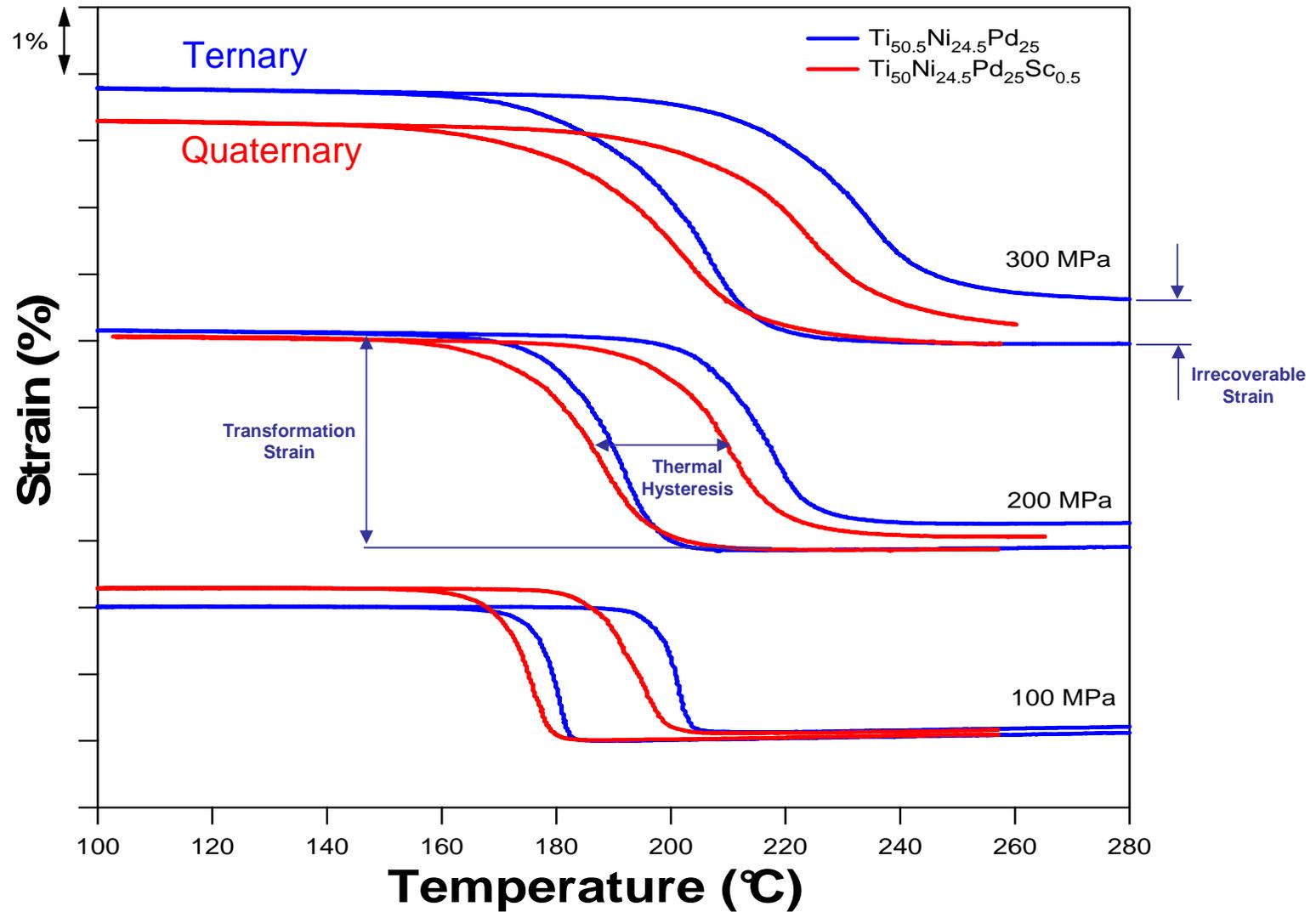
**1°C** peak shift per cycle after the 2<sup>nd</sup> cycle. **0.6°C** peak shift per cycle after the 2<sup>nd</sup> cycle.



# Thermo-mechanical Testing

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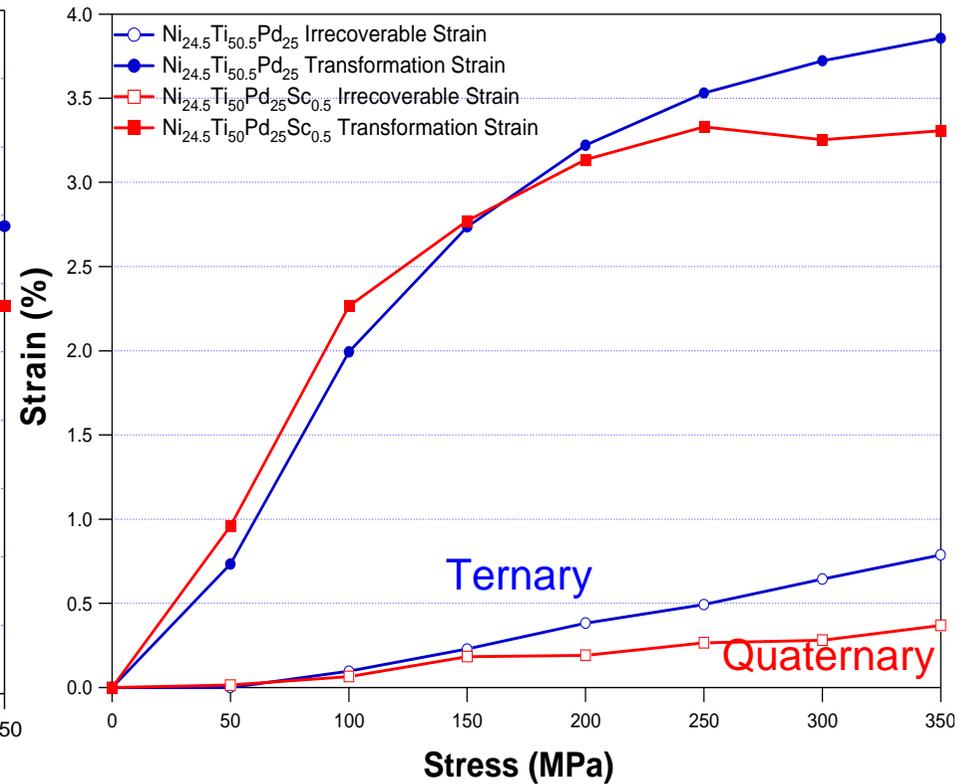
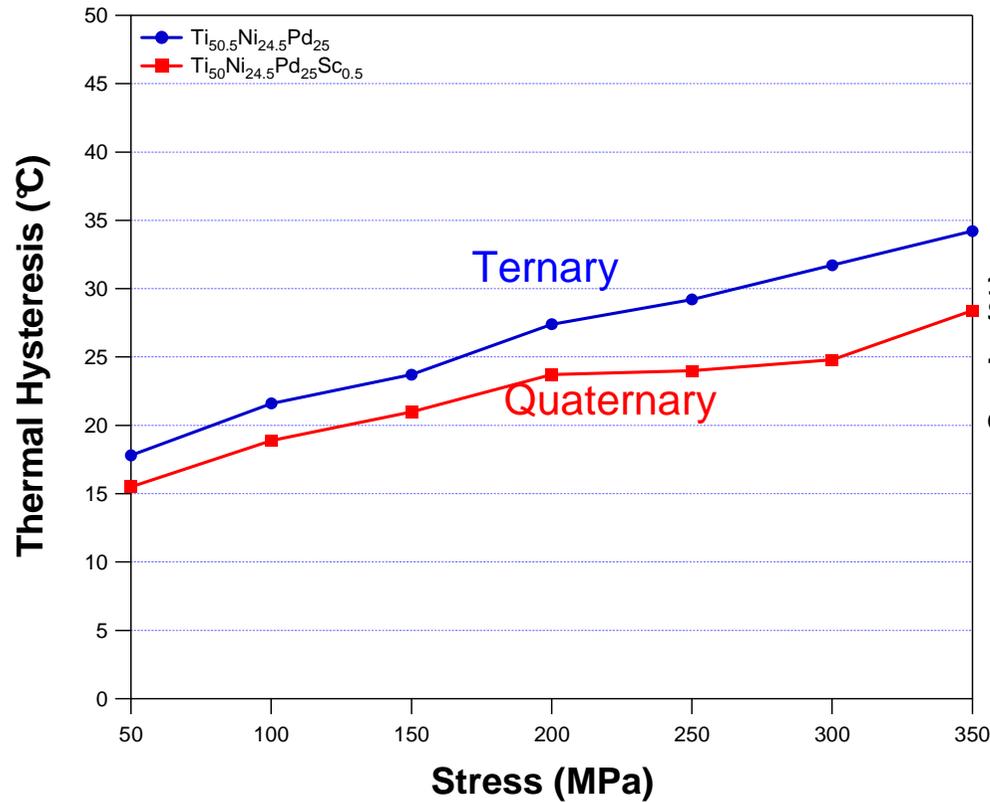




# Thermo-mechanical Testing

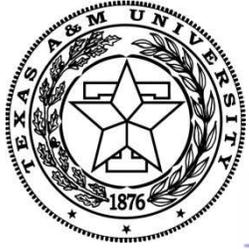
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## Addition of the quaternary element Sc:

- Decreases the amount of accumulated irrecoverable strain
- Decreases the thermal hysteresis
- Slightly decreases the transformation strain levels



# Experimental Results

## Part II

ECAE of  $\text{TiNiPd}_{25}\text{Sc}_{0.5}$

Heat Treatment of ECAE'ed  $\text{TiNiPd}_{25}\text{Sc}_{0.5}$



## ECAE Conditions

- 4E 425°C for  $\text{Ti}_{50}\text{Ni}_{24.5}\text{Pd}_{25}\text{Sc}_{0.5}$
- 4E 425°C for  $\text{Ti}_{49.5}\text{Ni}_{25}\text{Pd}_{25}\text{Sc}_{0.5}$

## Heat Treatment

300°C, 1 hour followed by air cooling

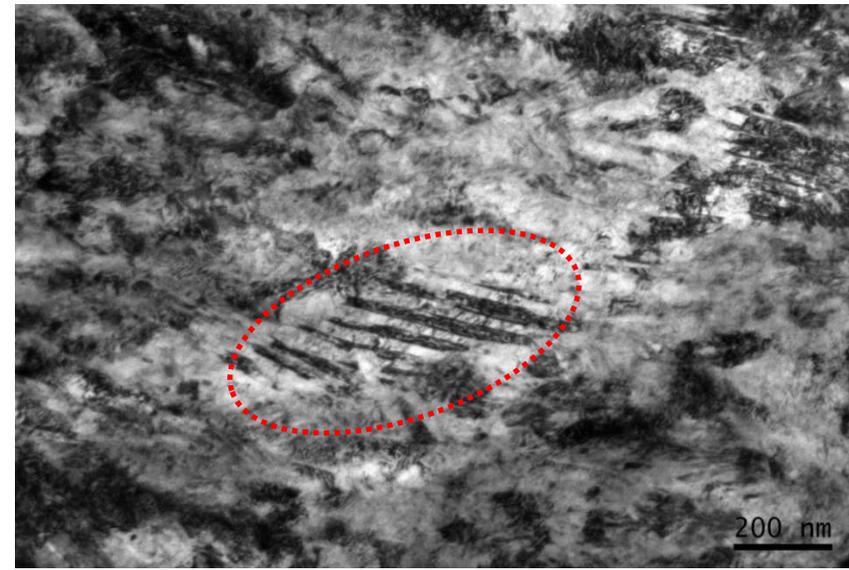
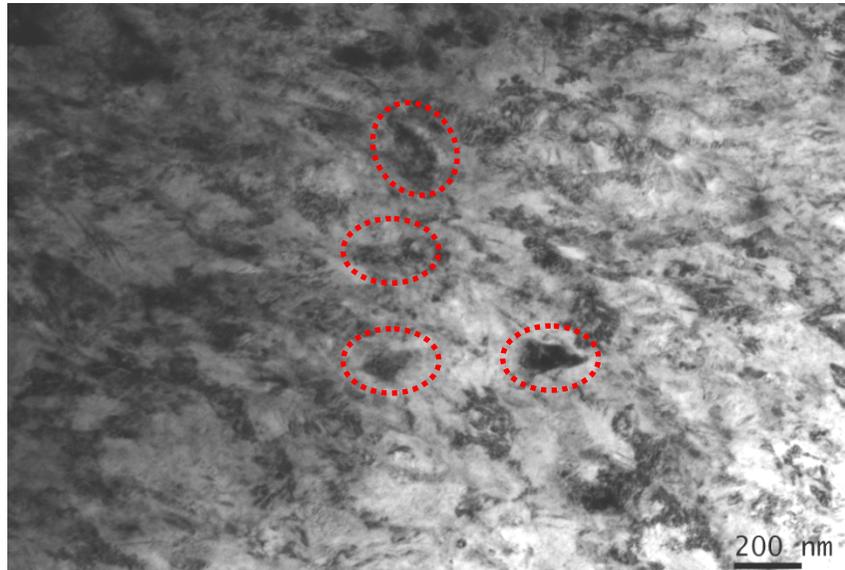


# Material Characterization

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ECAE'ed  $\text{Ti}_{50}\text{Ni}_{24.5}\text{Pd}_{25}\text{Sc}_{0.5}$ , RT



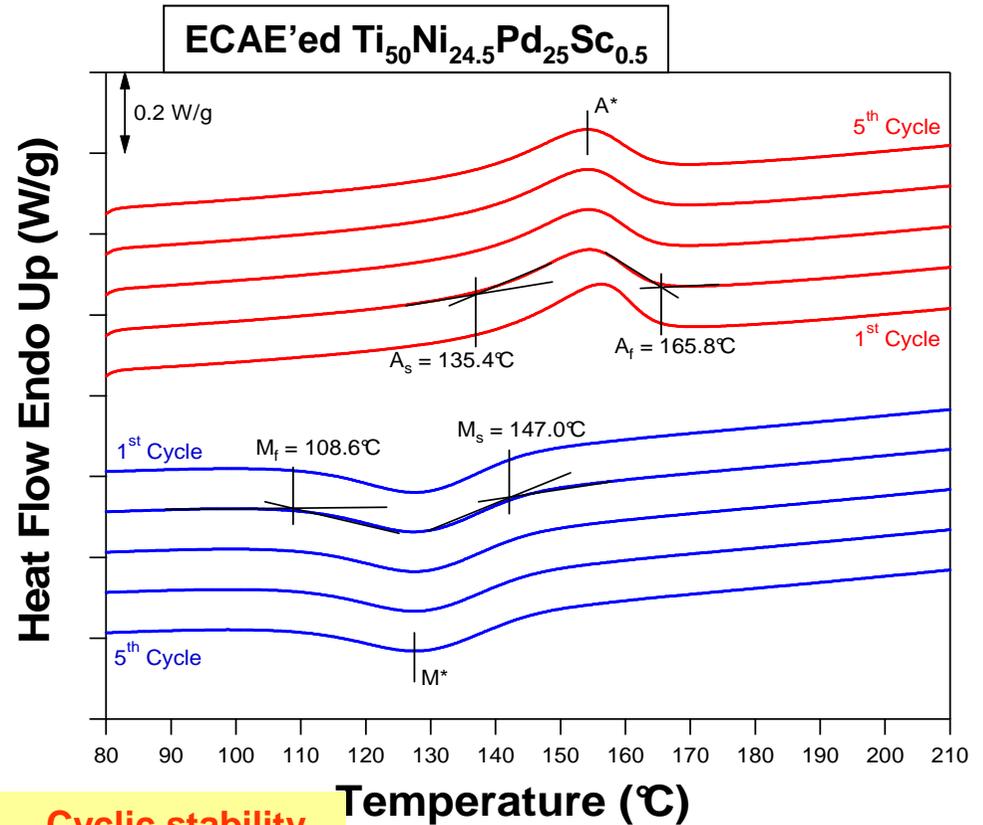
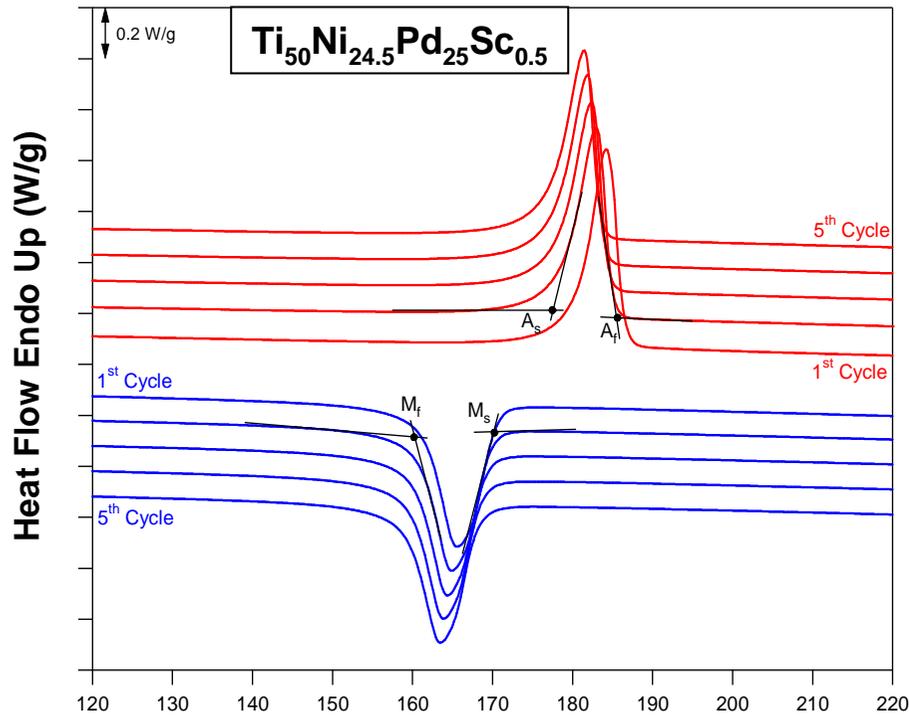
- Nano sized (150-200 nm) grains due to heavy deformation
- B19' martensite structure



# Thermo-mechanical Testing

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Temperature (°C)

Temperature (°C)

$M_s = 170.1^\circ\text{C}$

$A_f = 185.1^\circ\text{C}$

Transformation temperatures decreased further

Cyclic stability increased further

$M_s = 147.0.1^\circ\text{C}$

$A_f = 165.8^\circ\text{C}$

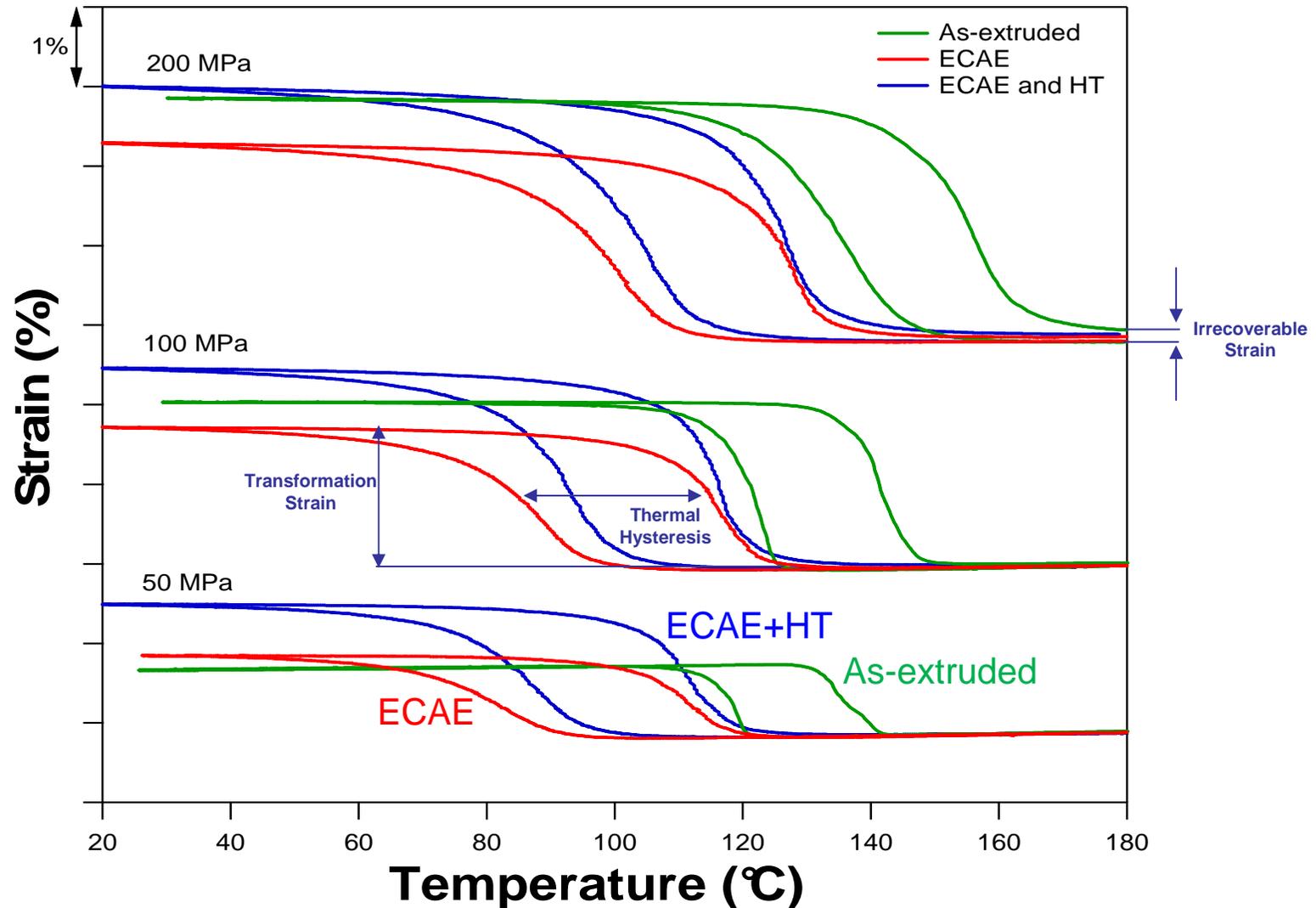
**0.6°C** peak shift per cycle after the 2<sup>nd</sup> cycle. **No** peak shift per cycle after the 2<sup>nd</sup> cycle.



# Thermo-mechanical Testing

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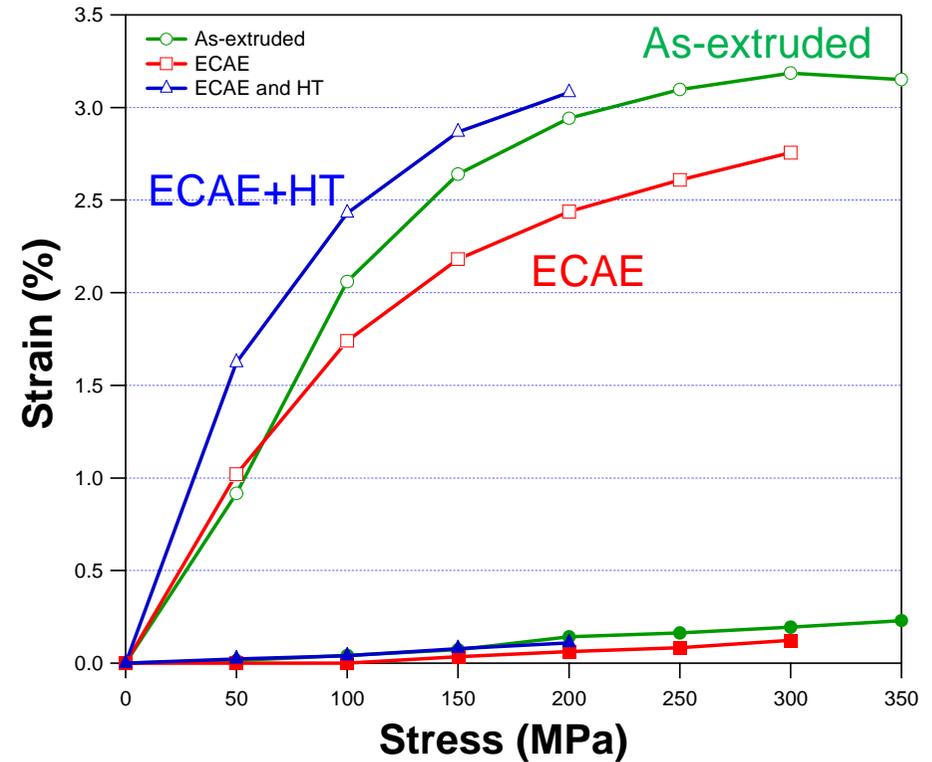
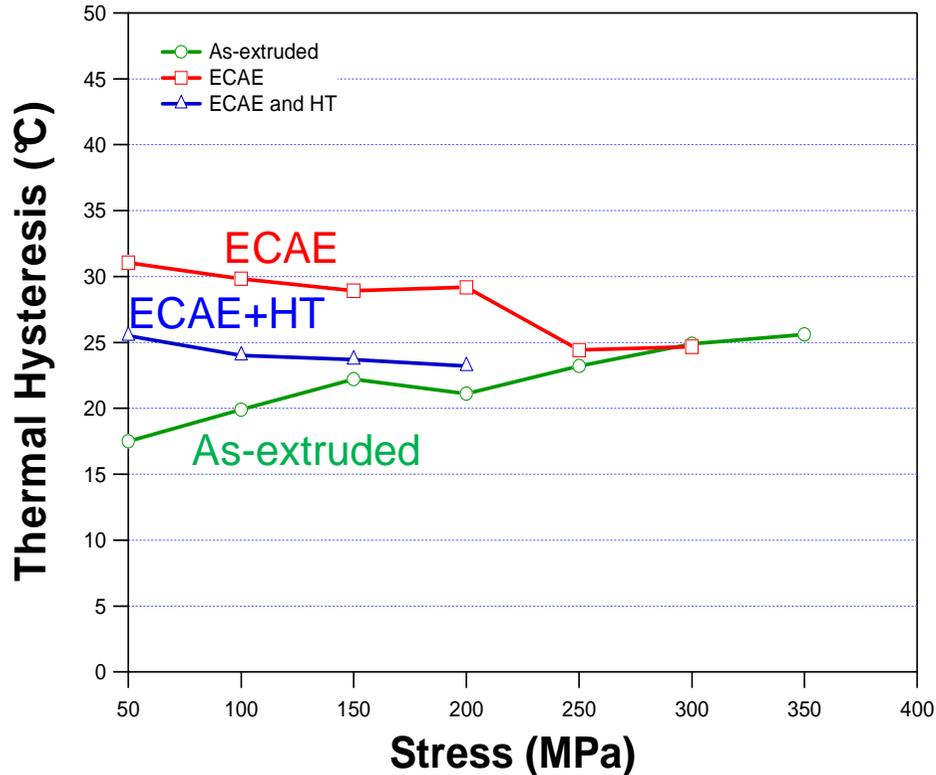




# Thermo-mechanical Testing

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Composition:  $\text{Ti}_{49.5}\text{Ni}_{25}\text{Pd}_{25}\text{Sc}_{0.5}$

- ECAE depresses the transformation temperatures
- ECAE decreases the amount of accumulated irrecoverable strain
- Heat treatment after ECAE increases the transformation temperatures and improves the strain output beyond that of the as-extruded material for a given stress level.



# Conclusions

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- Quaternary addition of Sc improved the shape memory properties of TiNiPd by improving thermal and mechanical cyclic stability.
- Quaternary addition of Sc changed the structure of martensite from B19 to B19'.
- ECAE followed by heat treatment further improved the shape memory properties of TiNiPdSc.
- Both methods can eliminate the necessity of costly and long training cycles before the HTSMA is used in an application.

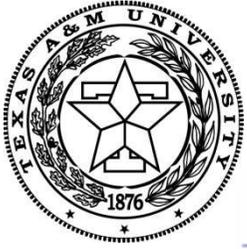


# Future Work

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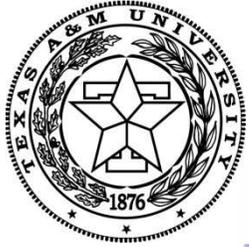
- Addition of different levels of Sc
- Different ECAE routes and heat treatments
- Isobaric thermal cyclic tests



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**Thank you!**



# Appendix

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Element	Atomic Number	Atomic weight (g/mol)	Density	Melting Point (°C)	Crystal Structure	Bond Length (pm)	Atomic radius (pm)	E (GPa)	G (GPa)	Hardness (B)
Titanium	22	47,867	4,506	1668	HCP	289,6	140	116	44	716
Nickel	28	58,693	8,908	1455	FCC	249,2	135	200	76	700
Palladium	46	106,42	12,023	1555	FCC	275,1	140	121	44	373 ?
Scandium	21	44,955	2,985	1541	HCP	321,2	160	74,4	29,1	750